

# Nicrofer<sup>®</sup> 5923 hMo - alloy 59

Material Data Sheet No. 4030  
December 2005 Edition

**Corrosion-resistant alloy**

<sup>®</sup> 5923 - alloy 59  
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Nicrofer<sup>®</sup> 5923 hMo - alloy 59  
Nicro

A company of  
ThyssenKrupp  
Stainless

**ThyssenKrupp VDM**



ThyssenKrupp

# Nicrofer® 5923 hMo – alloy 59

Nicrofer 5923 hMo is a nickel-chromium-molybdenum alloy with an extra-low carbon and silicon content. The alloy was developed by ThyssenKrupp VDM and has excellent corrosion resistance and high mechanical strength.

Nicrofer 5923 hMo is characterized by:

- outstanding resistance to a wide range of corrosive media under oxidizing and reducing conditions
- excellent resistance to pitting and crevice corrosion and freedom from chloride-induced stress-corrosion cracking
- excellent resistance to mineral acids, such as nitric, phosphoric, sulfuric and hydrochloric acids and in particular to sulfuric and hydrochloric acid mixtures
- excellent resistance to contaminated mineral acids
- good corrosion resistance to hydrochloric acid over the whole concentration range up to 40 °C (104 °F).
- good workability and weldability without susceptibility to hot cracking
- approval for pressure-vessel use with wall temperatures of –196 to 450 °C (–320 to 840 °F)
- approved in ISO 15156/MR0175, to the highest Test Level VII for sour gas service

## Designations and standards

Country	Material designation	Specification							
		Chemical composition	Tube and pipe		Sheet and plate	Rod and bar	Strip	Wire	Forgings
seamless	welded								
D DIN VdTÜV BAM*	W.-Nr. 2.4605 NiCr23Mo16Al  The alloy is listed in the BAM list for the transportation of dangerous goods	17744 505	17751		17750 505	17752 505	17750	17753	505
F AFNOR									
UK BS									
USA ASTM ASME	UNS N06059		B 622 SB-622	B 619/626 SB-619/626	B 575 SB-575	B 574 SB-574	B 575 SB-575		B 564 SB-564
ISO	Material listed in ISO 15156/MR0175								

\*BAM = Bundesanstalt für Material Forschung und Prüfung (Federal German Institute for Materials Research and Testing).

Table 1 – Designations and standards.

## Chemical composition

	Ni	Cr	Fe	C	Mn	Si	Mo	Co	Al	P	S
min.	bal.	22.0					15.0		0.1		
max.		24.0	1.5	0.010	0.5	0.10	16.5	0.3	0.4	0.015	0.005

Some compositional limits of other specifications may vary slightly.

Table 2 – Chemical composition (wt.-%) according to ASTM.

## Physical properties

Density	8.6 g/cm <sup>3</sup>	0.311 lb/in. <sup>3</sup>
Melting range	1310 – 1360 °C	2390 – 2480 °F
Permeability at 20 °C/68 °F (RT)	≤ 1.001	

Temperature (T)		Specific heat		Thermal conductivity		Electrical resistivity		Modulus of elasticity		Coefficient of thermal expansion between room temperature and T	
°C	°F	$\frac{J}{kg \cdot K}$	$\frac{Btu}{lb \cdot ^\circ F}$	$\frac{W}{m \cdot K}$	$\frac{Btu \cdot in.}{ft^2 \cdot h \cdot ^\circ F}$	$\mu\Omega \cdot cm$	$\frac{\Omega \cdot circ \text{ mil}}{ft}$	$\frac{kN}{mm^2}$	10 <sup>3</sup> ksi	$\frac{10^{-6}}{K}$	$\frac{10^{-6}}{^\circ F}$
20	68	414	0.099	10.4	72	126	758	210	30.5		
93	200		0.101		83		766		30.0		6.6
100	212	425		12.1		127		207		11.9	
200	392	434		13.7		129		200		12.2	
204	400		0.104		96		776		29.0		6.8
300	572	443		15.4		131		196		12.5	
316	600		0.106		105		788		28.3		7.0
400	752	451		17.0		133		190		12.7	
427	800		0.108		119		800		27.4		7.1
500	932	459		18.6		134		185		12.9	
538	1000		0.110		132		806		26.4		7.2
600	1112	464		20.4		133		178		13.1	

Table 3 – Typical physical properties at room and elevated temperatures.

## Mechanical properties

The following properties are applicable to Nicrofer 5923 hMo in the solution-treated condition and indicated size ranges.

Specified properties of material outside these size ranges are subject to special enquiry.

Product	Dimensions		Yield strength				Tensile strength		Elongation A <sub>5</sub> *
	mm	inches	R <sub>p0.2</sub> N/mm <sup>2</sup>	ksi	R <sub>p1.0</sub> N/mm <sup>2</sup>	ksi	R <sub>m</sub> N/mm <sup>2</sup>	ksi	
Sheet, strip* cr	0.5 – 6.4	0.018 – 0.25							
Plate hr	5.0 – 30	<sup>3</sup> / <sub>16</sub> – 1 <sup>3</sup> / <sub>16</sub>	340	49	380	55	690	100	40
Rod, bar, forgings	≤ 100	≤ 4							
Rod, bar, forgings	> 100	> 4	320	46	360	52	650	94	40

\*Elongation values for strip products are normally determined on an initial gauge length of 50 mm (2 in.). These values are lower, dependent on the alloy, than the corresponding A<sub>5</sub> values by an order of approx. 10%.

Table 4 – Minimum mechanical properties at room temperature according to VdTÜV data sheet 505.

# Nicrofer® 5923 hMo - alloy 59

Temperature (T)		Yield strength <sup>1)</sup>				Tensile strength <sup>2)</sup>		Elongation
°C	°F	R <sub>p0.2</sub>		R <sub>p1.0</sub>		R <sub>m</sub>		A <sub>5</sub>
		N/mm <sup>2</sup>	ksi	N/mm <sup>2</sup>	ksi	N/mm <sup>2</sup>	ksi	%
93	200		≥ 43		≥ 48		95 (91)	50
100	212	≥ 290		≥ 330		650 (620)		
200	392	≥ 250		≥ 290		615 (585)		
204	400		≥ 36		≥ 42		89 (85)	
300	572	≥ 220		≥ 260		580 (550)		
316	600		≥ 31		≥ 37		84 (80)	
400	752	≥ 190		≥ 230		545 (515)		
427	800		≥ 26		≥ 32		77 (74)	
450	842	≥ 175		≥ 215		525 (495)		

<sup>1)</sup> For plates above 30 mm and up to 50 mm (1<sup>3</sup>/<sub>16</sub> to 2 in.) thickness the yield strength values should be reduced by 20 N/mm<sup>2</sup> (3 ksi).  
<sup>2)</sup> Values for rods in brackets.

Table 5 – Mechanical properties at elevated temperatures according to VdTÜV data sheet 505 for thicknesses up to 30 mm (1<sup>3</sup>/<sub>16</sub> in.).

Material temperatures		Forgings, rod, sheet & plate, strip	
°C	°F	N/mm <sup>2</sup>	ksi
38	100		25.0
93	200		25.0
100	212	172	
149	300		24.7
200	392	161	
204	400		23.3
260	500		22.0
300	572	147	
316	600		20.9
343	650		20.4
371	700		19.8
399	750		19.4
400	752	134	

For welded tube and pipe a factor of 0.85 should be applied.

Table 6 – Maximum allowable stress values according to ASME.

### ISO V-notch impact toughness

Average values at RT: ≥ 225 J/cm<sup>2</sup>  
 at -196 °C (-320 °F): ≥ 200 J/cm<sup>2</sup>

One of the main reasons why nickel alloys are selected is for their performance under corrosive conditions. Though sometimes underestimated, characteristic design data frequently also plays an important role in selecting a particular alloy. As Fig. 1 shows,  $R_{p0.2}$  yield strength data for Nicrofer 5923 hMo is up to 20% higher than that of other similar alloys. This allows for a corresponding reduction in wall thickness which results in less material usage and thus in a more cost-effective design.

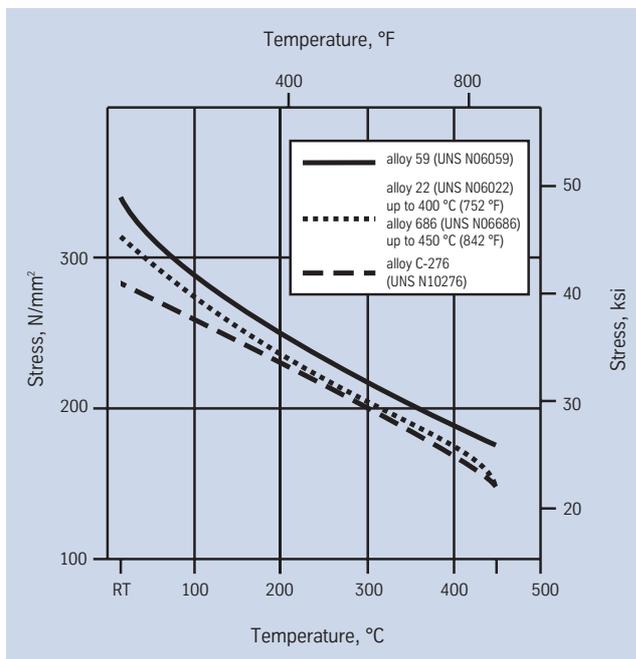


Fig. 1 –  $R_{p0.2}$  yield strength of Nicrofer 5923 hMo in comparison with other nickel alloys.

### Metallurgical structure

Nicrofer 5923 hMo has a face-centered-cubic structure.

### Corrosion resistance

The nickel-chromium-molybdenum alloy Nicrofer 5923 hMo with extremely low silicon and carbon contents is not prone to grainboundary precipitation during hot forming or welding. The alloy is therefore suitable for many chemical process applications in both oxidizing and reducing media.

Because of its high nickel, chromium and molybdenum contents, the alloy exhibits excellent resistance to attack by chloride ions.

Most standardized corrosion tests relate to oxidizing conditions, under which Nicrofer 5923 hMo has been demonstrated to be superior to other Ni-Cr-Mo alloys. However, the favorable behavior of Nicrofer 5923 hMo in some reducing media such as, for example, boiling 10% sulfuric acid, in which Nicrofer 5923 hMo exhibits a corrosion rate more than three times lower than that of other well established Ni-Cr-Mo alloys, suggests also promising prospects for the use of this material in reducing media in the CPI. The excellent corrosion resistance of Nicrofer 5923 hMo in hydrochloric acid is shown in Fig. 3.

Optimum corrosion resistance can be obtained only if the material is in the correct metallurgical condition and possesses a clean structure.

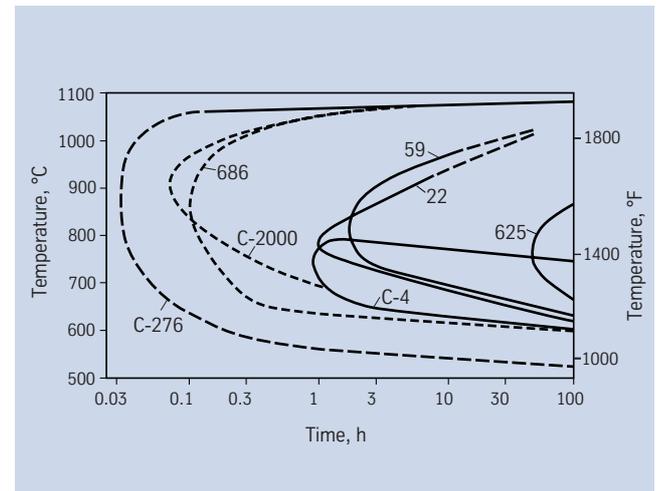


Fig. 2 – Time-temperature-sensitization (TTS) diagrams of nickel-chromium-molybdenum alloys tested according to ASTM G-28 A. Areas to the right of the curves indicate intergranular corrosion  $>50\mu\text{m}$  (.002 in.)

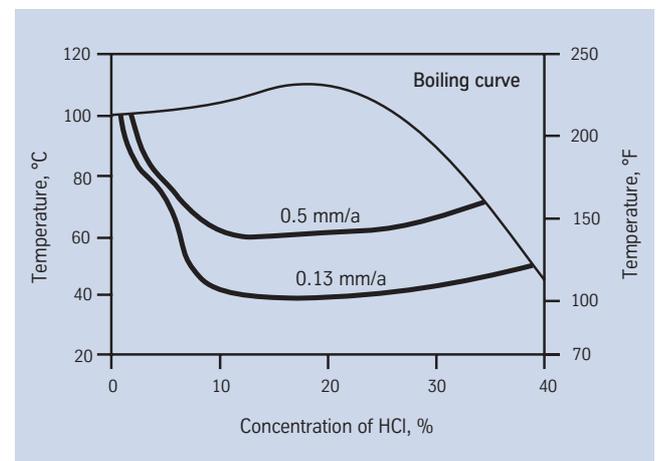


Fig. 3 – Isocorrosion diagram of Nicrofer 5923 hMo in hydrochloric acid based on static immersion test results.

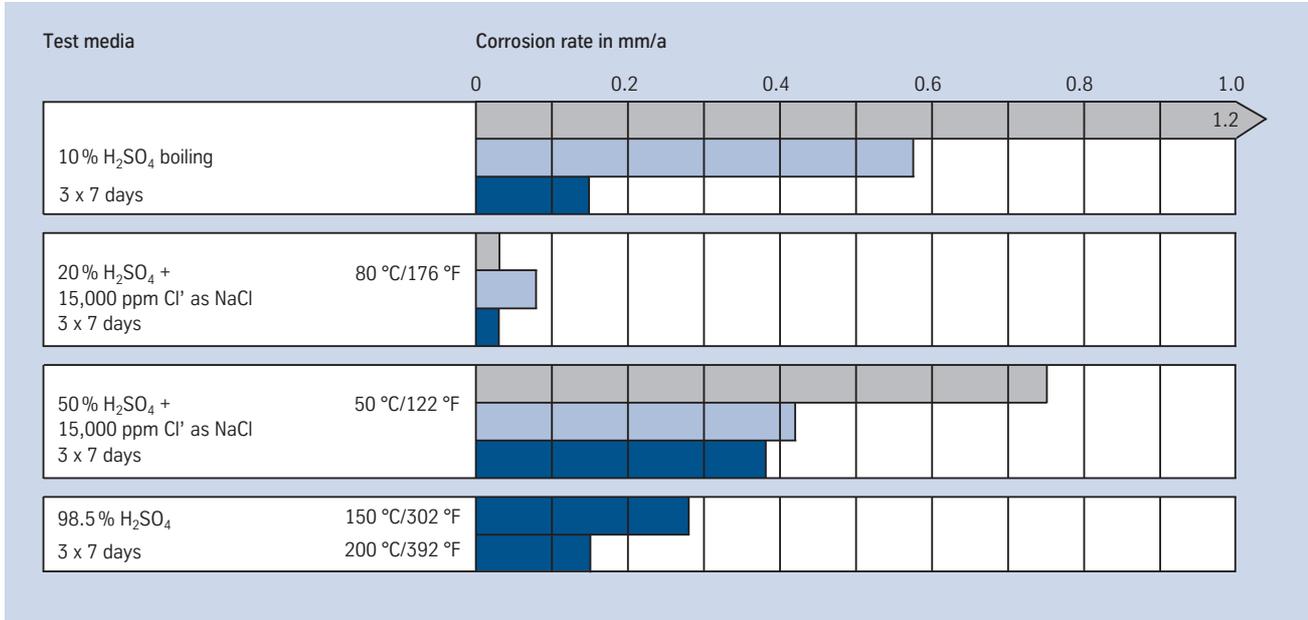


Fig. 4 – Comparison of corrosion rates in a variety of environments:  
alloy 625 █, alloy C-276 █, Nicrofer 5923 hMo █.

Alloy	Normal range of corrosion rates in mm/a according to	
	ASTM G-28 A	ASTM G-28 B
Nicrofer 5923 hMo – alloy 59	0.6 - 1.0	0.08 - 0.15
Nicrofer 5621 hMoW – alloy 22	0.8 - 1.2	0.10 - 0.15
Nicrofer 5716 hMoW – alloy C-276	4.0 - 9.2	0.80 - 1.20

Table 7 – Comparison of typical corrosion rates in ASTM G-28 A and B standardized corrosion tests.

Alloy	CPT	CCT
Nicrofer 5923 hMo – alloy 59	> 120 °C / > 248 °F	110 °C / 230 °F
Nicrofer 5621 hMoW – alloy 22	120 °C / 248 °F	105 °C / 221 °F
Nicrofer 5716 hMoW – alloy C-276	115 – 120 °C / 239 – 248 °F	105 °C / 221 °F
Nicrofer 6020 hMo – alloy 625	100 °C / 212 °F	85 – 95 °C / 185 – 203 °F

Above 120 °C the "Green Death" solution breaks down chemically.

Table 8 – Critical pitting temperature (CPT) and crevice corrosion temperature (CCT) in 'Green Death' test solution.  
(7 vol.% H<sub>2</sub>SO<sub>4</sub> + 3 vol.% HCl + 1% CuCl<sub>2</sub> + 1% FeCl<sub>3</sub> after repeated immersion for 24 hours using 5 °C (9 °F) temperature increments).

### Applications

Nicrofer 5923 hMo has a wide range of applications in the chemical, petrochemical and pharmaceutical industry, in energy production and in pollution control equipment.

Typical applications are:

- components in organic processes involving chlorides, particularly when acid chloride catalysts are employed
- digesters and bleaching plants in the pulp and paper industry
- scrubbers, heat exchangers, dampers, wet fans and spraying systems for flue gas desulfurization (FGD) in fossil-fired power stations and waste incineration plants
- equipment and components in sour gas service
- reactors for acetic acid and acetic anhydride
- sulfuric acid coolers

### Fabrication and heat treatment

Nicrofer 5923 hMo can readily be hot and cold worked and machined.

#### Heating

Workpieces must be clean and free from all kinds of contaminants before and during any heat treatment.

Nicrofer 5923 hMo may become impaired if heated in the presence of contaminants such as sulfur, phosphorus, lead and other low-melting-point metals. Sources of such contaminants include marking and temperature-indicating paints and crayons, lubricating grease and fluids and fuels.

Fuels must be as low in sulfur as possible. Natural gas should contain less than 0.1 wt.-% sulfur. Fuel oils with a sulfur content not exceeding 0.5 wt.-% are suitable.

Due to their close control of temperature and freedom from contamination, thermal treatments in electric furnaces under vacuum or an inert gas atmosphere are to be preferred. Treatments in an air atmosphere and alternatively in gas-fired furnaces are acceptable though, if contaminants are at low levels so that a neutral or slightly oxidizing furnace atmosphere is attained. A furnace atmosphere fluctuating between oxidizing and reducing must be avoided as well as direct flame impingement on the metal.

#### Hot working

Nicrofer 5923 hMo may be hot worked in the temperature range 1180 to 950 °C (2160 to 1740 °F). Cooling after hot working should be by water quenching.

Heat treatment after hot working is recommended to ensure maximum corrosion resistance.

For heating up workpieces should be charged into the furnace at maximum working temperature (solution annealing temperature).

#### Cold working

For cold working the material should be in the annealed condition. Nicrofer 5923 hMo has a higher work-hardening rate than austenitic stainless steels. This should be taken into account when selecting forming equipment.

Interstage annealing may be necessary with high degrees of cold forming. After cold working with more than 15% deformation solution annealing is required before use.

#### Heat treatment

Solution heat treatment should be carried out in the temperature range 1100 to 1180 °C (2010 to 2160 °F), preferably at about 1120 °C (2050 °F).

Water quenching or rapid air cooling for thicknesses above 1.5 mm (0.06 in.) is recommended and is essential for maximum corrosion resistance.

For any thermal treatment the material should be charged into the furnace at temperature. Also for any thermal treatment operation the precautions concerning cleanliness mentioned earlier under 'Heating' must be observed.

#### Descaling and pickling

Oxides of Nicrofer 5923 hMo and discoloration adjacent to welds are more adherent than on stainless steels. Grinding with very fine abrasive belts or discs is recommended. Care should be taken to prevent tarnishing.

Before pickling which may be performed in a nitric/hydrofluoric acid mixture with proper control of pickling time and temperature, the surface oxid layer must be broken up by abrasive blasting, by carefully performed grinding or by pretreatment in a fused salt bath.

#### Machining

Nicrofer 5923 hMo should be machined in solution-treated condition. As the alloy exhibits a high work-hardening rate only low cutting speeds should be used compared with low-alloyed standard austenitic stainless steels. An adequate depth of cut is important in order to cut below the previously formed work-hardened zone. Tools should be engaged at all times.

#### Welding

When welding nickel alloys, the following instructions should be adhered to:

#### Workplace

The workplace should be in a separate location, well away from the areas where carbon steel fabrication takes place. Maximum cleanliness and avoidance of draughts are paramount.

#### Auxiliaries, clothing

Clean fine leather gloves and clean working clothes should be used.

#### Tools and machinery

Tools used for nickel alloys and stainless steels must not be used for other materials. Brushes should be made of stainless material. Fabricating and working machinery such as shears, presses or rollers should be fitted with means (felt, cardboard, plastic sheet) of avoiding contamination of the metal with ferrous particles, which can be pressed into the surface and thus lead to corrosion.

### Cleaning

Cleaning of the base metal in the weld area (both sides) and of the filler metal (e. g. welding rod) should be carried out with ACETONE.

Trichlorethylene (TRI), perchlorethylene (PER), and carbon tetrachloride (TETRA) must not be used.

### Edge preparation

This should preferably be done by mechanical means, i. e., by turning, milling or planing; abrasive water jet or plasma cutting is also suitable. However, in the latter case the cut edge (the face to be welded) must be finished off cleanly. Careful grinding without overheating is permissible.

### Included angle

The different physical characteristics of nickel alloys and special stainless steels compared with carbon steel generally manifest themselves in a lower thermal conductivity and a higher rate of thermal expansion. This should be allowed for by means of, among other things, wider root gaps or openings (1–3 mm), while larger included angles (60–70°), as shown in Fig. 5, should be used for individual butt joints owing to the viscous nature of the molten weld metal and to counteract the pronounced shrinkage tendency.

### Striking the arc

The arc should only be struck in the weld area, i. e., on the faces to be welded or on a run-out piece. Striking marks lead to corrosion.

### Welding process

Nicrofer 5923 hMo can be joined to itself and to many other metals by conventional welding processes. These include GTAW (TIG), plasma arc, GMAW (MIG/MAG and MAG-Tandem) and SMAW (MMA). Pulsed arc welding is the preferred technique. For the MAG processes the use of a multi-component shielding gas (Ar+He+H<sub>2</sub>+CO<sub>2</sub>) is recommended.

For welding, Nicrofer 5923 hMo should be in the annealed condition and be free from scale, grease and markings. When welding the root, care should be taken to achieve best-quality root backing (argon 99.99), so that the weld is free from oxides after welding the root. Any heat tint should be removed preferably by brushing with a stainless steel wire brush while the weld metal is still hot.

### Filler metal

For the gas-shielded welding processes, filler metal with the same composition as the base metal is recommended:

Bare electrodes: Nicrofer S 5923 – FM 59 (W.-No. 2.4607)  
UNS N06059  
AWS A5.14: ERNiCrMo-13  
DIN EN ISO 18274: S Ni 6059 (NiCr23Mo16)

Covered electrodes: W.-No. 2.4609  
UNS W86059  
AWS A5.11: ENiCrMo-13  
DIN EN ISO 14172: E Ni 6059 (NiCr23Mo16)

For overlay welding by the electro-slag method (RES):

Weld strip: Nicrofer B 5923 – WS 59 (W.-No. 2.4607)  
UNS N06059  
AWS A5.14: ERNiCrMo-13  
DIN EN ISO 18274: B Ni 6059 (NiCr23Mo16)

### Welding parameters and influences (heat input)

Care should be taken that the work is performed with a deliberately chosen, low heat input as indicated in Table 10 by way of example. Use of the stringer bead technique should be aimed at. Interpass temperature should be kept below 150 °C (300 °F).

The welding parameters should be monitored as a matter of principle.

The heat input Q may be calculated as follows:

$$Q = \frac{U \times I \times 60}{v \times 1000} \text{ (kJ/cm)}$$

U = arc voltage, volts  
I = welding current, amps  
v = welding speed, cm/min.

Consultation with ThyssenKrupp VDM's Welding Laboratory is recommended.

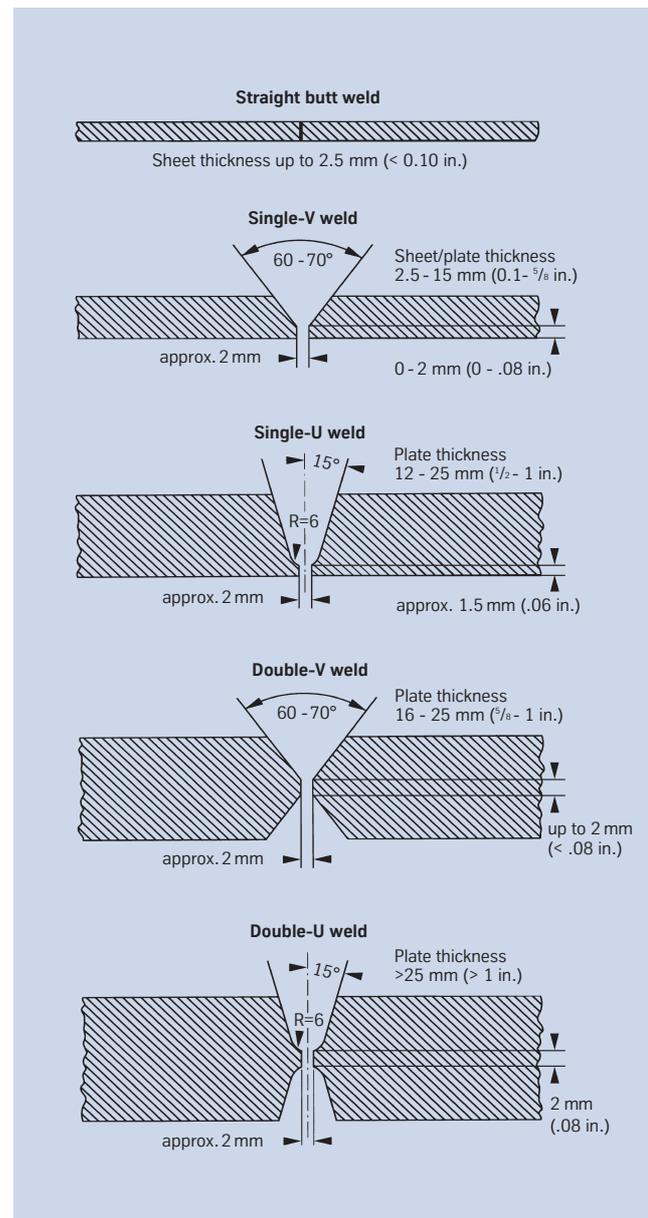


Fig. 5 – Edge preparation for welding of nickel alloys and special stainless steels.

Sheet/ plate thick- ness mm	Welding process	Filler metal		Welding parameters				Welding speed  cm/min.	Shielding gas Type & rate  l/min.	Plasma- gas Type & rate  l/min.
		diameter	speed	Root pass		Intermediate and final passes				
		mm	m/min.	I A	U V	I A	U V			
3.0	Manual GTAW	2.0		90	10	110 – 120	11	approx. 15	Ar W3 <sup>1)</sup> 8 – 10	
6.0	Manual GTAW	2.0 – 2.4		100 – 110	10	120 – 140	12	14 – 16	Ar W3 <sup>1)</sup> 8 – 10	
8.0	Manual GTAW	2.4		100 – 110	11	130 – 140	12	14 – 16	Ar W3 <sup>1)</sup> 8 – 10	
10.0	Manual GTAW	2.4		100 – 110	11	130 – 140	12	14 – 16	Ar W3 <sup>1)</sup> 8 – 10	
3.0	Autom. GTAW	1.2	approx. 1.2	Manual GTAW		150	11	25	Ar W3 <sup>1)</sup> 12 – 14	
5.0	Autom. GTAW	1.2	approx. 1.4	Manual GTAW		180	12	25	Ar W3 <sup>1)</sup> 12 – 14	
2.0	Hot wire GTAW	1.0				180	11	80	Ar W3 <sup>1)</sup> 12 – 14	
10.0	Hot wire GTAW	1.2		Manual GTAW		220	12	40	Ar W3 <sup>1)</sup> 12 – 14	
4.0	Plasma arc	1.2	approx. 1.0	approx. 180	25			30	Ar W3 <sup>1)</sup> 30	Ar 4.6 3.0
6.0	Plasma arc	1.2	approx. 1.0	200 – 220	26			26	Ar W3 <sup>1)</sup> 30	Ar 4.6 3.5
8.0	GMAW (MIG/MAG <sup>2)</sup> )	1.0	6 – 7	Manual GTAW		130 – 140	23 – 27	24 – 30	Ar 4.6 <sup>2)</sup> 18	
10.0	GMAW (MIG/MAG <sup>2)</sup> )	1.2	6 – 7	Manual GTAW		130 – 150	23 – 27	25 – 30	Ar 4.6 <sup>2)</sup> 18	
6.0	SMAW (MMA)	2.5		40 – 70	approx. 21	40 – 70	approx. 21			
8.0	SMAW (MMA)	2.5 – 3.25		40 – 70	approx. 21	70 – 100	approx. 22			
16.0	SMAW (MMA)	4.0				90 – 130	approx. 22			

<sup>1)</sup> Argon or argon + max. 3% hydrogen

<sup>2)</sup> For MAG welding the use of the multi-component shielding gas Cronigon Ni10, for example, is recommended.

In all gas-shielded welding operations, ensure adequate back shielding with Ar 4.6.

Figures are for guidance only and are intended to facilitate setting of the welding machines.

Table 9 – Welding parameters (guide values).

Welding process	Heat input per unit length kJ/cm	Welding process	Heat input per unit length kJ/cm
GTAW, manual, fully mechanised	max. 8	GMAW, MIG/MAG, manual, fully mechanised	max. 8
Hot wire GTAW	max. 6	SMAW, manual metal arc (MMA)	max. 7
Plasma arc	max. 10		

Table 10 – Heat input per unit length (guide values).

**Postweld treatment**

(brushing, pickling and thermal treatments)

Brushing with a stainless steel wire brush immediately after welding, i.e. while the metal is still hot generally results in removal of heat tint and produces the desired surface condition without additional pickling.

Pickling, if required or prescribed, however, would generally be the last operation performed on the weldment. Also refer to the information on 'Descaling and pickling'.

Neither pre- nor postweld thermal treatments are required.

**Availability**

Nicrofer 5923 hMo is available in the following standard product forms:

**Sheet & plate**

(for cut-to-length availability, refer to strip)

Conditions:

hot or cold rolled (hr, cr),  
thermally treated and pickled

Thickness mm	hr / cr	Width <sup>1)</sup> mm	Length <sup>1)</sup> mm
1.10 – < 1.50	cr	2000	8000
1.50 – < 3.00	cr	2500	8000
3.00 – < 7.50	cr / hr	2500	8000
7.50 – ≤ 25.00	hr	2500	8000 <sup>2)</sup>
> 25.00 <sup>1)</sup>	hr	2500 <sup>2)</sup>	8000 <sup>2)</sup>

inches		inches	inches
0.043 – < 0.060	cr	80	320
0.060 – < 0.120	cr	100	320
0.120 – < 0.300	cr / hr	100	320
0.300 – ≤ 1.000	hr	100	320 <sup>2)</sup>
> 1.000 <sup>1)</sup>	hr	100 <sup>2)</sup>	320 <sup>2)</sup>

<sup>1)</sup> other sizes subject to special enquiry<sup>2)</sup> depending on piece weight**Discs and rings**

Conditions:

hot rolled or forged,  
thermally treated,  
descaled or pickled or machined

Available up to a maximum piece weight of 6 t for discs and 3 t for rings in accordance to drawings and technical feasibility.

**Rod & bar**

Conditions:

forged, rolled, drawn,  
thermally treated,  
descaled or pickled, machined, peeled or ground

Product	Forged <sup>1)</sup> mm	Rolled <sup>1)</sup> mm	Drawn <sup>1)</sup> mm
Rod (o. d.)	≤ 600	8 – 100	12 – 65
Bar, square (a)	40 – 600	15 – 280	not standard
Bar, flat (a x b)	(40 – 80) x (200 – 600)	(5 – 20) x (120 – 600)	(10 – 20) x (30 – 80)
Bar, hexagonal (s)	40 – 80	13 – 41	≤ 50

	inches	inches	inches
Rod (o. d.)	≤ 24	<sup>5</sup> / <sub>16</sub> – 4	<sup>1</sup> / <sub>2</sub> – 2 <sup>1</sup> / <sub>2</sub>
Bar, square (a)	1 <sup>5</sup> / <sub>8</sub> – 24	<sup>10</sup> / <sub>16</sub> – 11	not standard
Bar, flat (a x b)	(1 <sup>5</sup> / <sub>8</sub> – 3 <sup>1</sup> / <sub>8</sub> ) x (8 – 24)	( <sup>3</sup> / <sub>16</sub> – <sup>3</sup> / <sub>4</sub> ) x (4 <sup>3</sup> / <sub>4</sub> – 24)	( <sup>3</sup> / <sub>8</sub> – <sup>3</sup> / <sub>4</sub> ) x (1 <sup>1</sup> / <sub>4</sub> – 3 <sup>1</sup> / <sub>8</sub> )
Bar, hexagonal (s)	1 <sup>5</sup> / <sub>8</sub> – 3 <sup>1</sup> / <sub>8</sub>	<sup>1</sup> / <sub>2</sub> – 1 <sup>5</sup> / <sub>8</sub>	≤ 2

<sup>1)</sup> other sizes and conditions subject to special enquiry**Forgings**

Shapes other than discs, rings, rod and bar are subject to special enquiry. Flanges and hollow shafts may be available up to a piece weight of 10 t.

**Strip<sup>1)</sup>**

Conditions:

cold rolled,  
thermally treated and pickled or bright annealed<sup>2)</sup>.

Thickness mm	Width <sup>3)</sup> mm	Coil I. D. mm		
0.02 – ≤ 0.10	4 – 200 <sup>4)</sup>	300	400	
> 0.10 – ≤ 0.20	4 – 350 <sup>4)</sup>	300	400	500
> 0.20 – ≤ 0.25	4 – 750		400	500 600
> 0.25 – ≤ 0.60	6 – 750		400	500 600
> 0.60 – ≤ 1.0	8 – 750		400	500 600
> 1.0 – ≤ 2.0	15 – 750		400	500 600
> 2.0 – ≤ 3.0	25 – 750		400	500 600

inches	inches	inches		
0.0008 – ≤ 0.004	0.16 – 8 <sup>4)</sup>	12	16	
> 0.004 – ≤ 0.008	0.16 – 14 <sup>4)</sup>	12	16	20
> 0.008 – ≤ 0.010	0.16 – 30		16	20 24
> 0.010 – ≤ 0.024	0.20 – 30		16	20 24
> 0.024 – ≤ 0.040	0.32 – 30		16	20 24
> 0.040 – ≤ 0.080	0.60 – 30		16	20 24
> 0.080 – ≤ 0.120	1.0 – 30		16	20 24

<sup>1)</sup> Cut-to-length available in lengths from 250 to 4000 mm (10 to 158 in.)<sup>2)</sup> Maximum thickness: bright annealed - 3 mm (0.120 in.)

cold rolled only - 3.5 mm (0.140 in.)

<sup>3)</sup> Wider widths subject to special enquiry<sup>4)</sup> Wider widths up to 730 mm (29 in.) subject to special enquiry.

**Wire****Conditions:**

bright drawn, 1/4 hard to hard, bright annealed

**Dimensions:**

0.1 – 12.0 mm (0.004 – 0.47 in.) diameter,  
in coils, pay-off packs, on spools and spiders

**Welding filler metals**

Suitable welding rods, wire, strip electrodes and electrode core wire are available in standard sizes.

**Seamless tube and pipe**

Using ThyssenKrupp VDM cast materials seamless tubes and pipes are produced and available from DMV STAINLESS Deutschland GmbH, Wiesenstr. 36, D-45473 Mülheim/Ruhr; (Tel.: +49 208 458-2611; Fax: +49 208 458-2641; EMail: salesgermany@dmv-stainless.com); Internet: www.dmv-stainless.com).

**Welded tube and pipe**

Welded tubes and pipes are obtainable from qualified manufacturers using ThyssenKrupp VDM semi-fabricated products.

**Technical publications**

The following publications concerning Nicrofer 5923 hMo – alloy 59 may be obtained from ThyssenKrupp VDM GmbH:

**VDM Report No. 17:**

Wallpaper installation guidelines and other fabrication procedures for FGD maintenance, repair and new construction with VDM high-performance nickel alloys – June 1991

**M. Jasner, W. Herda, M. Rockel:**

Crevice corrosion behaviour of high-alloyed austenitic steels and nickel-base alloys in seawater, determined under various test conditions;

Applications of Stainless Steel 92, Lohf. Proc., Stockholm, pp. 446 – 457 (1992)

**VDM Report No. 18:**

Corrosion-resistant materials for Flue Gas Desulphurisation systems – February 1993

**VDM Report No. 22:**

Behaviour of some metallic materials in sulphuric acid – August 1994

**VDM Report No. 23:**

Alloying effects and innovations in nickel base alloys for combating aqueous corrosion – February 1996

**VDM Case History No. 1:**

The lining of four flue-gas scrubbers with Nicrofer 5923 hMo – alloy 59 in a German waste incineration plant – October 1995

**VDM Case History No. 2:**

Boxberg III – The successful retrofitting of an Eastern German brown coal fired power station using Nicrofer 5923 hMo - alloy 59 – May 1997

**VDM Case History No. 3:**

Schkopau – First East German power plant using supercritical steam-cycle technology – February 1998

**VDM Case History No. 4:**

Nicrofer High-performance alloys for shut-off and regulating systems in modern fossil-fired power stations and waste-to-energy plants – May 1999

**VDM Case History No. 5:**

Nicrofer 5923 hMo - Alloy 59: A high-performance material for the chemical process industries – May 2000

**D. C. Agarwal, W. R. Herda, J. Klöwer:**

Case Histories on Solving Severe Corrosion Problems in the CPI and other Industries by an advanced Ni-Cr-Mo Alloy 59 (UNS N06059); CORROSION 2000, Paper No. 00501, NACE International, Houston, 2000.

**D. C. Agarwal, J. Klöwer:**

Nickel Base Alloys: Corrosion Challenges in the New Millennium; CORROSION 2001, Paper No. 01325, NACE International, Houston, 2001.

**D. C. Agarwal, G. K. Grossmann:**

Case Histories on the use of Nickel Alloys in Municipal & Hazardous Waste Fueled Facilities; CORROSION 2001, Paper No. 01177, NACE International, Houston, 2001.

**D. C. Agarwal, U. Brill, R. A. Corbett:**

Results of Various Tests on Welded and Unwelded alloy 59 for Rad-Waste Containers; CORROSION 2001, Paper No. 01120, NACE International, Houston, 2001.

**FGD Corrosion Problems & Solutions: Past, Present and Future Outlook;**

US EPA/EPRI/DOE Mega Symposium, Arlington, IL, August 2001.

Application case histories of Ni-Cr-Mo and 6Mo alloys in the petrochemical and chemical process industries; Stainless Steel World, May 2002.

**D. C. Agarwal, U. Brill, R. Behrens;**

Alloy 59: UNS N06059, provides answers to many critical problems of the marine industry: Crevice Corrosion, Weld repair, SCC of Fasteners; CORROSION 2004, Paper No. 04281, NACE International, Houston, 2004.

**D. C. Agarwal, R. Behrens:**

Results of various corrosion and mechanical tests on cold reduced bars of alloy 59, UNS N06059, for fastener applications; CORROSION 2005, Paper No. 05231, NACE International, Houston, 2005.

**D. C. Agarwal:**

New application of the utmost advanced superalloy 59 in flue gas desulfurization; ThyssenKrupp techforum, July 2005.

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Nicrofer

hM

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